Patent Application of

David G.Wuchinich

for

Longitudinal-Torsional Ultrasonic Tissue Dissection

BACKGROUND-CROSS REFERENCES TO RELATED APPLICATIONS

This application is based on United States provisional application No. 60/196,357 filed April 12, 2000.

BACKGROUND-FIELD OF INVENTION

This invention describes the use of mechanical resonant longitudinal-torsional vibration to dissect biological tissue.

BACKGROUND-DESCRIPTION OF PRIOR ART

The use of ultrasonic vibration to separate tissue was disclosed by Balamuth (U.S. Patent No 3,526,219) in 1970 who showed a variety of surgical instruments equipped with tips for different applications in the dissection of biological tissue. His devices provided motion either parallel, also known as longitudinal, motion or

perpendicular, known as transverse motion, to tissue surface. Kelman and Banko (U.S. Patent No. 3,589,363) disclosed in 1971 apparatus and methods for dissecting and simultaneously aspirating tissue with a device that provided longitudinal tip contacting motion. Broadwin and Weiss (U.S. Patent No. 4,136,700) later developed an aspirating ultrasonic tissue dissector that utilized transverse tip motion. Kelman (U.S. Patent No. 4,504,264) and the Wuchinich (U.S. Patent No. 5,176,677) patented ultrasonic dissectors that utilized, in additional to ultrasonic longitudinal tip motion, transverse ultrasonic tip motion with motor driven rotation to enhance tissue removal. Wuchinich (U.S. Patent No. 4,750,902) also patented apparatus for the endoscopic dissection of tissue, combining the use of longitudinal ultrasonic vibration with aspiration, irrigation, telescopic vision and electro-cauterization.

Chief among the limitations of ultrasonic tissue dissection has been its feeble ability to separate collagenous tissue, bone and other connective or structurally supportive tissue. However, because ultrasonic vibration offers precise control and very little heat and collateral damage, attempts have been repeatedly made to improve its performance on tissue otherwise resistant to its effect. Wuchinich shows one such invention (U.S. Patent No. 5,176,677) for using transverse ultrasonic motion in combination with rotation to cut collagenous tissue such as cartilage and the meniscus.

All of the devices and methods that have been disclosed have not accomplished the object of rapid, precise removal of tissue normally resistant to ultrasonic dissection. Furthermore, although instruments that incorporate rotation of the tip, do offer improved performance on resistant tissue because they require rotating seals and bearing they are complicated in construction, expensive to manufacture and fragile in use.

In 1970 Teumin described the development of and experiments with ultrasonic longitudinal-torsional resonators, known as L-T resonators. These ultrasonic devices are capable of transforming longitudinal motion into both longitudinal and torsional motion within one and same structure. Applications described by Teumin include welding and drilling. These resonators are also distinguished in converting imparted longitudinal motion from a transducer into both longitudinal and torsional motion at the tip of the L-T resonator. Such imparted longitudinal motion may be generated by any of the many common inexpensive electro-mechanical transducers for providing this motion by mechanical connection of such a transducer to the longitudinal torsional resonator. In 1981 Kleesatel (U.S. Patent No. 4,281,987) connected a transducer providing longitudinal motion to an L-T resonator for the purpose of generating continuous rotary motion.

The resonators described by Teumin were made by creating an inhomogeneous cross section along the length of an otherwise uniform bar and then twisting the bar along its length. One way to create an inhomogeneous cross section to place grooves along the length of what was otherwise a round bar to create flutes. The resonator is then physically twisted about its axis, spiraling the grooves. The twisted bar was then connected to a transducer that produced longitudinal motion in response to application of an electrical current and voltage. The same structure can be obtained, and was evaluated by Teumin, by using a conventional twist drill or by machining the grooves into the bar. L-T resonators can also be made by twisting a bar with a rectangular cross section about its axis to produce a spiral in exactly the way that drills were first made.

The flat twisted bar L-T resonator has the advantages of simplicity and economy in construction and can sustain greater torsional motion because the mass of the cross section remains uniformly distributed along its width. The mass of the cross section of the grooved twisted bar L-T resonator increases along its width

or radius with the result that stress produced by torsional motion through the same angle is greater in this bar than in the flat twisted bar.

In 2000 Boukhny (U.S. Patent No. 6,077,285) showed apparatus for providing both longitudinal and torsional ultrasonic tip for the purpose of enhancing tissue dissection. His device utilizes separate torsional and longitudinal transducers to provide this motion. As such, simultaneous operation of both transducers is described as providing both longitudinal and torsional motion of the working tip. However this system requires two electrical generators to supply the power, one each for each of the different transducers. Furthermore, all such devices, whether longitudinal, transverse or torsional must be fixed within an enclosure, such as a handpiece, preferably at points where there is no motion, known as motional nodes. However, because the wavelength of torsional and longitudinal vibration is, in general, substantially different, the node or nodes for longitudinal vibration and torsional motion will, in general, be located at different points on the transducer and other portions of other resonators attached to the transducers. Hence, in general, no true motionless point may be found with the result that either longitudinal or torsional motion will be communicated to the handpiece and thereby to the operator holding the handpiece. Although vibration isolators can be utilized to prevent the communication of such unintended motion, if they are truly isolating they invariably complicate construction of the device and, if simple, consume power in the form of heat generated by contact with a moving surface. Hence, Boukhn's device is both complicated to operate, needing two separate power sources, and difficult to construct.

BRIEF DESCRIPTION OF THE INVENTION

The invention described herein permits the efficacious dissection of tissue resistant to longitudinal or transverse vibration or a combination of longitudinal and transverse vibration by providing simultaneously longitudinal and torsional

ultrasonic motion to a tissue contacting tip through the use of longitudinal-torsional resonators.

The invention has the further object of providing such longitudinal-torsional vibration using only one type of electro-mechanical transducer, either torsional or longitudinal and thereby simplifying the construction of ultrasonic dissection apparatus.

The invention has another object in permitting the application of longitudinal-torsional motion to tissue dissection using established, well-known and inexpensive electro-mechanical transducers heretofore developed for generating longitudinal motion.

Other objects, features and advantages of the invention will become apparent with reference to the drawings and the following description of the drawings, invention and claims.

BRIEF DESCRIPTON OF THE DRAWINGS

Figure 1 is a block diagram illustrating the principal components of an ultrasonic tissue dissecting system incorporating L-T resonators.

Figure 2 is shaded isometric view of an example of an L-T knife tip ultrasonic dissector.

Figure 3 is a shaded isometric view of an example of an L-T dissecting, and aspirating ultrasonic dissector.

Figure 4 is an example of an ultrasonic L-T tissue dissector utilizing a torsional transducer and having a twisted section interposed between the transducer and the tip.

REFERENCE NUMERALS IN DRAWINGS

1	Torsional or Longitudinal Ultrasonic Transducer
2	L-T Resonator
3	Tissue Contacting Tip
4	Irrigation Conduit to L-T Resonator
5	Vacuum Conduit to L-T Resonator
6	Vacuum conduit to Longitudinal or Torsional Ultrasonic Transducer
7	Vacuum Valves
8	Irrigation Conduit to Longitudinal or Torsional Ultrasonic Transducer
9	Vacuum Conduit to Tissue/Fluid Collection Receptacle
10	Tissue/Fluid Collection Receptacle
11	Vacuum Pump
12	Irrigation Pump and Valves
13	Irrigation Conduit to Irrigation Pump and Valves
14	Irrigation Solution Container
15	Ultrasonic Generator
16	Electrical Connection to Ultrasonic Longitudinal or Torsional Transducer
17	Vacuum Conduit to Vacuum Valves
18	Tissue
19	Ultrasonic Longitudinal Transducer
20	Voltage and Current applied to Ultrasonic Longitudinal Transducer
21	L-T resonator
22	Tissue contact point of L-T resonator
23	Transducer Longitudinal Motion

24   L-T motion at Tissue Contact point

25   Low motion region of Ultrasonic Longitudinal Transducer

26   Low motion region of L-T resonator

28   Coil

33   Slot in L-T Resonator

35   Axial hole in L-T resonator

41   Inhomogeneous portion of L-T resonator

40   Torsional motion of Torsional Ultrasonic Transducer

43   Piezo-electric torsional elements

44   Low motion region of Torsional Ultrasonic Transducer

45   Irrigation fluid

46   Piezo-electric longitudinal elements

47   First Electrical connection

48   Second Electrical connection

DETAILED DESCRIPTION OF THE INVENTION

The principal components of a system suitable for ultrasonic tissue dissection is shown in **Figure 1** along with their interconnection. Referring now to **Figure 1**, an electro-mechanical transducer **1** that receives alternating electrical current and voltage through connections **16** from an ultrasonic generator **15** produces an alternating mechanical vibration at its point of mechanical contact with longitudinal torsional resonator **2**. The longitudinal torsional resonator, receiving this vibration from the transducer by direct mechanical contact with transducer **1**, produces in a tissue contacting tip longitudinal-torsional vibration. This tip **3** contacts tissue 18 for the purpose of dissection.

Electro-mechanical transducer **1** may produce either longitudinal or torsional motion in response to the supply of electrical energy. The tissue contacting tip **3**

may be an integral part of the L-T resonator **2** or a separate, mechanically attached component.

Irrigation fluid **45** in container **14** is conveyed to either the transducer **1** or the L-T resonator **2** through a pump and valve control system **12** and conduits **13**, **8** and **4** or other appliances suitable for fluid conveyance.

A vacuum pump **11** provides suction by connecting line **9** to a tissue and fluid receptacle **10** and thereby through connecting conduit **17** to control valves **7** and hence by connecting line **6** to the transducer or by connecting line **5** to the L-T resonator.

In operation, vibration, irrigation and suction may be present at the transducer or L-T resonator simultaneously, individually or in any combination.

The functions and utility of irrigation, suction which is also known as aspiration and vibration in dissecting tissue has been fully described by Banko (U.S. Patent No. 3,589,363) and Broadwin (U.S. Patent No. 4,136,700), both of which patents are incorporated herein by reference.

In **Figure 2** an electro-mechanical transducer **19** is shown mechanically connected to an L-T resonator **21** having an inhomogeneous cross sectional region **41** and mechanically joined to knife tissue contacting tip **22**. The mechanical connection between the L-T resonator and the transducer and the L-T resonator and the tip may be made by any of the common methods known in the art such by screw threads, press fit, welding, brazing or the connection may be metallurgically continuous. Transducer 19 contains piezo-electric elements **46** which change their dimensions in response the application of an electric field and to which first and second connection wires **47** and **48**, forming part of connections

shown as **16** in **Figure 1** are attached. Transducer **19** produces, in response to the application of alternating current and voltage **20,** a longitudinal vibration **23** at the point of connection to L-T resonator **26**. The transducer **19** also possesses a rim **26** on which there is little or no vibration present and which therefore constitutes a region suitable for mounting or holding the transducer **19** in a stationary structure such as a handpiece. The L-T resonator may also contain a portion of its structure, shown as item **28**, where there is also little or no mechanical vibration and which is again suitable for further securing it to a stationary object.

The L-T resonator converts the longitudinal vibration **23** into a longitudinal-torsional vibration **24** at tip **22**. The ratio of the magnitude of the longitudinal-torsional vibration **24** to the longitudinal vibration **23**, represented in **Figure 2** as the length of the double-ended arrow lines, may be any number greater than zero, but preferably lies in the range of 1 to 100.

As Teumin has described, for the L-T resonator **21** to produce a torsional component of motion comparable to the longitudinal component a substantial portion, shown as item **41** in the drawings, of the cross sectional mass must be made inhomogeneous. If this inhomogeneity is made by twisting a flat bar or grooving a round one, this inhomogeneity should preferentially made in the portion of the bar subjected to maximum stress. As previously referenced, to minimize the stress produced in the inhomogeneous portion of the resonator, in the preferred embodiment of this invention, the inhomogeneity is created by twisting a bar of rectangular cross section about its axis. Normally this portion of the bar can be found using the stress distribution that would take place if the bar were not twisted. Such stress distributions have been described by Merkulov and are available to practitioners skilled in the art. In addition, as Teumin has shown, an L-T resonator made by twisting a bar may be joined to another untwisted bar having a larger cross sectional area than the twisted bar to form a stepped half

wavelength resonator as described by Wuchinich (U.S. Patent No. 5,811,909). In such a construction, a connection made to the transducer at the available end of the untwisted bar will produce at the end of the twisted bar longitudinal-torsional motion greater in magnitude than that at the point of contact with the transducer.

The portion of the resonator containing the cross sectional inhomogeneity may also be tapered, as shown in **Figure 2**, from a larger cross section at the end connecting to the transducer to a smaller cross section at the opposite end to again produce an increase in the longitudinal and torsional components of motion. Eisner has described a variety of tapers suitable for the purpose and known in the art.

It also possible to create the inhomogeneity necessary to produce longitudinal-torsional vibration from a longitudinal or torsional vibration by making the material of the bar itself inhomogeneous. For example, if the density or elasticity of the bar is made to vary in a helical manner along the length of the bar, longitudinal or torsional vibration at one end of the bar will be converted in to longitudinal-torsional vibration at the other end.

To both dissect and aspirate tissue, the L-T resonator may be made with a hollow passage that communicates with a similar hollow passage in the transducer or with a fitting attached to tubing or other tissue and fluid carrying devices.

In **Figure 3** an electro-mechanical transducer **19** is mechanically attached to an L-T resonator **21**. The transducer **19** contains a magnetostrictive element **29** which changes its dimensions in response to the application of a magnetic and which vibrates longitudinally with magnitude and direction shown as item **23** in response to a voltage and current **20** applied to coil **28** which generates the magnetic field. The portion **41** of the L-T resonator that contains an

inhomogeneous cross section also contains a hole **35** through its length which communicates with slot **33**, thereby permitting connections in the slot to fluid lines **4** or **5** of **Figure 1** to either a source of irrigation fluid or suction as shown by Banko (U.S. Patent No. 3,589,363) and Wuchinich (U.S. Patent 4,063,557) which are herein incorporated by reference. Wuchinich also shows an alternative fluid connection to the transducer (U.S. Patent No. 4,750,902) again incorporated herein by reference. The tissue contacting tip part of, or attached to, the L-T resonator **22** vibrates longitudinally and torsionally with a magnitude **24** shown. The ratio of the vibration magnitude **24** to the transducer magnitude **23**, taken as the ratio of the lengths of respective double arrowhead lines, can be any value greater than 0, but preferably lies within the range of 1 and 100.

Figure 4 shows an electro-mechanical torsional transducer **43** mechanically joined to an L-T resonator **21** having a knife tissue contacting tip **22**. Transducer **43** contains piezo-electric elements **42** to which first and second connecting wires **47** and **48** respectively, forming part of the connections identified as item **16** in **Figure 1,** are attached. Transducer **43** produces, in response to the application of alternating current and voltage **20,** a torsional vibration **40** at the point of connection to the L-T resonator. The transducer **43** also possesses a rim **44** on which there is little or no vibration present and which therefore constitutes a region suitable for mounting or holding the transducer **43** in a stationary structure such as a handpiece. The L-T resonator contains a section with an inhomogeneous cross sectional portion **41** between two sections of uniform cross section. The tissue contacting portion **22** of the L-T resonator **21** executes, in response to the torsional vibration **40** produced by transducer **43** a longitudinal – torsional vibration **24**. The ratio of this vibration to that of the transducer, taken as the length of the double ended arrowhead line may be any value greater than 0, but preferably lies within the range of 1 and 100.